

Class C Amplifier Calculations With The Aid of Constant-Current Characteristics

In calculating and predicting the operation of a vacuum tube as a class-C radio frequency amplifier, the considerations which determine the operating conditions are plate efficiency, power output required, maximum allowable grid and plate dissipation, maximum allowable plate voltage and maximum allowable plate current. The values chosen for these factors will depend both on the demands of a particular application and the tube selected to do the job.

The plate and grid currents of a class-C amplifier are periodic pulses, the durations of which are always less than 180 degrees. For this reason the average plate and grid currents, power output, driving power, etc., cannot be directly calculated but must be determined by a Fourier analysis from points selected along the line of operation as plotted on the constant-current characteristics. This may be done either analytically or graphically. While the Fourier analysis has the advantage of accuracy, it also has the disadvantage of being tedious and involved.

An approximate analysis which has proven to be sufficiently accurate for most purposes is presented in the following material. This system has the advantage of giving the desired information at the first trial. The system, which is an adaption of a method developed by Wagener¹, is direct because the important factors, power output, plate efficiency and plate voltage may be arbitrarily selected at the beginning.

In the material which follows, the following set of symbols will be used. These symbols are illustrated graphically in Figure 1.

Symbols

- P_i = Plate power input
- P_o = Plate power output
- P_p = Plate dissipation
- n = Plate efficiency expressed as a decimal
- E_{bb} = D-c plate supply voltage
- $E_{p_{m}}$ = Peak fundamental plate voltage
- $e_{b_{min}}$ = Minimum instantaneous plate voltage
- I_b = Average plate current
- $I_{b_{m}}$ = Peak fundamental plate current
- $i_{b_{max}}$ = Maximum instantaneous plate current
- θ_p = One-half angle of plate current flow
- E_{cc} = D-c grid bias voltage (a negative quantity)

- E_{gm} = Peak fundamental grid excitation voltage
- $e_{c_{mp}}$ = Maximum positive instantaneous grid voltage
- I_c = Average grid current
- $i_{c_{max}}$ = Maximum instantaneous grid current
- P_d = Grid driving power (including both grid and bias losses)
- P_g = Grid dissipation
- μ = Amplification factor

Method

The first step in the use of the system to be described is to determine the power which must be delivered by the class-C amplifier. In making this determination it is well to remember that ordinarily from 5 to 10 per cent of the power delivered by the amplifier tube or tubes will be lost in well-designed tank and coupling circuits at frequencies below 20 Mc. Above 20 Mc. the tank and coupling circuit losses are ordinarily somewhat above 10 per cent.

The plate power input necessary to produce the required output is determined by the plate efficiency:

$$P_i = \frac{P_o}{n}$$

For most applications it is desirable to operate at the highest possible efficiency. High-efficiency operation usually requires less expensive tubes and power supplies, and the amount of artificial cooling needed is frequently less than for low-efficiency operation. On the other hand, high-efficiency operation often requires more driving power and higher operating plate voltages. Eimac triodes will operate satisfactorily at 80 per cent efficiency at the highest recommended plate voltages and at 75 per cent efficiency at medium plate voltages.

The first determining factor in selecting a tube or tubes for any particular application is the maximum allowable plate dissipation. The total plate dissipation rating for the number of tubes used must be equal to or greater than that calculated from

$$P_p = P_i - P_o$$

After selecting a tube or tubes to meet the power output and plate dissipation requirements it becomes necessary to determine from the tube characteristics whether the tube selected is capable of the required operation and, if so, to determine the driving power, grid bias and grid current.

¹ W. G. Wagener, "Simplified Methods for Computing Performance of Transmitting Tubes," *Proc. I.R.E.*, Vol. 25, p. 47, (Jan. 1937).

The complete procedure necessary to determine the class-C-amplifier operating conditions is as follows²:

1. Select plate voltage, power output and efficiency.
2. Determine plate input from

$$P_i = \frac{P_o}{\eta}$$

3. Determine plate dissipation from

$$P_p = P_i - P_o$$

P_p must not exceed maximum rated plate dissipation for tube or tubes selected.

4. Determine average plate current from

$$I_b = \frac{P_i}{E_{bb}}$$

I_b must not exceed maximum rated plate current for tube selected.

5. Determine approximate i_{bmax} from

$$\begin{aligned} i_{bmax} &= 4.5I_b \text{ for } \eta = 0.80 \\ i_{bmax} &= 4.0I_b \text{ for } \eta = 0.75 \\ i_{bmax} &= 3.5I_b \text{ for } \eta = 0.70 \end{aligned}$$

6. Locate the point on constant-current characteristics where the constant plate current line corresponding to the approximate i_{bmax} determined in step 5 crosses the line of equal plate and grid voltages ("diode line"). Read e_{bmin} at this point.³

7. Calculate E_{pm} from

$$E_{pm} = E_{bb} - e_{bmin}$$

8. Calculate the ratio $\frac{I_{pm}}{I_b}$ from

$$\frac{I_{pm}}{I_b} = \frac{2\eta E_{bb}}{E_{pm}}$$

9. From the ratio of $\frac{I_{pm}}{I_b}$ calculated in step 8 determine the ratio $\frac{i_{bmax}}{I_b}$ from Chart 1.

10. Calculate a new value for i_{bmax} from ratio found in step 9.

$$i_{bmax} = (\text{ratio from step 9}) I_b$$

11. Read e_{cmp} and i_{cmax} from constant current characteristics for values of e_{bmin} and i_{bmax} determined in steps 6 and 10.

12. Calculate the cosine of one-half the angle of plate current flow from

$$\cos \theta_p = 2.3 \left(\frac{I_{pm}}{I_b} - 1.57 \right)^4$$

13. Calculate the grid bias voltage from

$$E_{cc} = \frac{1}{1 - \cos \theta_p} \left[\cos \theta_p \left(\frac{E_{pm}}{\mu} - e_{cmp} \right) - \frac{E_{bb}}{\mu} \right]$$

14. Calculate the peak fundamental grid excitation voltage from

$$E_{gm} = e_{cmp} - E_{cc}$$

15. Calculate the ratio $\frac{E_{gm}}{E_{cc}}$ for values of E_{cc} and E_{gm} found in steps 13 and 14.

16. Read ratio $\frac{i_{cmax}}{I_c}$ from Chart 2 for ratio $\frac{E_{gm}}{E_{cc}}$ found in step 15.

17. Calculate average grid current from ratio found in step 16 and value of i_{cmax} found in step 11.

$$I_c = \frac{i_{cmax}}{\text{ratio from step 16}}$$

18. Calculate approximate grid driving power from

$$P_d = 0.9 E_{gm} I_c^5$$

19. Determine grid dissipation from

$$P_g = P_d + E_{cc} I_c$$

P_g must not exceed the maximum rated grid dissipation for the tube selected.

Example

A typical application of this procedure is shown in the example below.

1. Desired power output..... 1250 watts
Desired plate voltage..... 4000 volts
Desired plate efficiency..... 75 per cent ($\eta = 0.75$)

$$2. \quad P_i = \frac{1250}{0.75} = 1670 \text{ watts}$$

$$3. \quad P_p = 1670 - 1250 = 420 \text{ watts}$$

Try type 450TL; Max. $P_p = 450W$; $\mu = 18$

$$4. \quad I_b = \frac{1670}{4000} = 0.417 \text{ ampere}$$

(Max. I_b for 450TL = 0.600 ampere)

5. Approximate $i_{bmax} = 4.0 \times 0.417 = 1.67$ ampere

$$6. \quad e_{bmin} = 315 \text{ volts (see figure 2)}$$

$$7. \quad E_{pm} = 4000 - 315 = 3685 \text{ volts}$$

$$8. \quad \frac{I_{pm}}{I_b} = \frac{2 \times 0.75 \times 4000}{3685} = 1.63$$

$$9. \quad \frac{i_{bmax}}{I_b} = 3.45 \text{ (from Chart 1)}$$

$$10. \quad i_{bmax} = 3.45 \times 0.417 = 1.44 \text{ amperes}$$

$$11. \quad e_{cmp} = 280 \text{ volts}$$

$$i_{cmax} = 0.330 \text{ amperes}$$

(see figure 3)

$$12. \quad \cos \theta_p = 2.32 (1.63 - 1.57) = 0.139$$

$$13. \quad E_{cc} = \frac{1}{1 - 0.139} \left[0.139 \left(\frac{3685}{18} - 280 \right) - \frac{4000}{18} \right] = -270 \text{ volts}$$

$$14. \quad E_{gm} = 280 - (-270) = 550 \text{ volts}$$

$$15. \quad \frac{E_{gm}}{E_{cc}} = \frac{550}{-270} = -2.04$$

$$16. \quad \frac{i_{cmax}}{I_c} = 5.69 \text{ (from Chart 2)}$$

$$17. \quad I_c = \frac{0.330}{5.69} = 0.058 \text{ amperes}$$

$$18. \quad P_d = 0.9 \times 550 \times 0.058 = 28.7 \text{ watts}$$

$$19. \quad P_g = 28.7 + (-270 \times 0.058) = 13.0 \text{ watts}$$

(Max P_g for 450TL = 65 watts)⁶

² In the case of push-pull or parallel amplifier tubes the analysis should be carried out on the basis of a single tube, dividing P_i , P_o and P_p by the number of tubes before starting the analysis and multiplying I_b , I_c and P_d by the same factor after completing the analysis.

³ In a few cases the lines of constant plate current will deflect sharply upward before reaching the diode line. In these cases e_{bmin} should not be read at the diode line but at the point where the plate current line intersects a line drawn from the origin through these points of inflection.

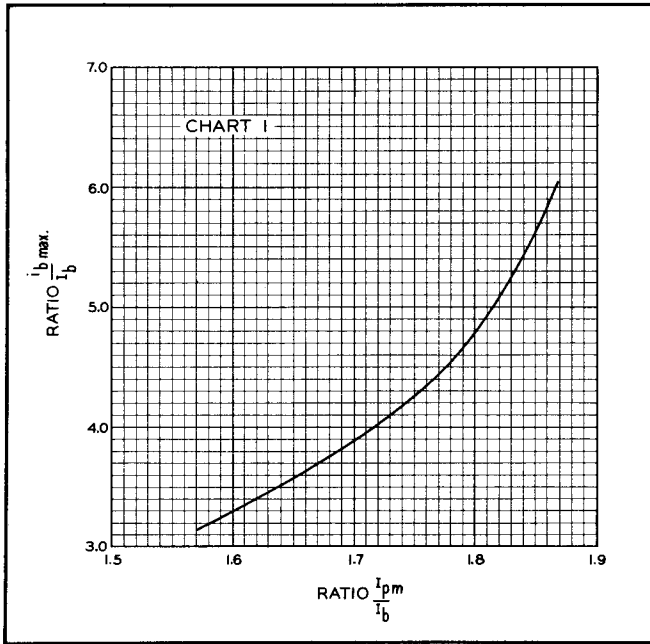


Chart 1

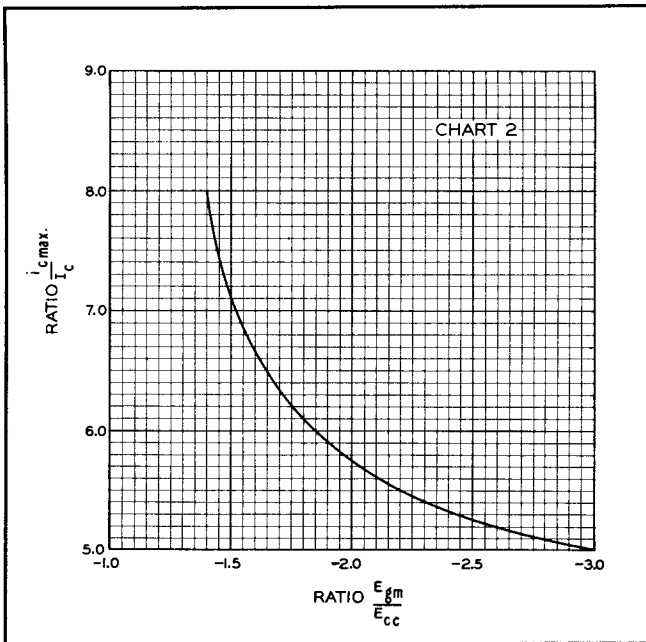


Chart 2

Nomographs

This system of class-C amplifier analysis is now being converted to nomograph form for presentation in the near future.

4 If this calculation gives $\cos \theta_p$ as zero or a negative quantity class-B operation is indicated and new operating conditions should be chosen on a basis of higher efficiency (less plate dissipation, more power output or less power input).

5 The calculated driving power is that actually used in supplying the grid and bias losses. Suitable allowance in driver design must be made to allow for losses in the coupling circuits between the driver plate and the amplifier grid.

6 "Vacuum Tube Ratings" Eimac News, Industrial Edition, Jan. 1945.

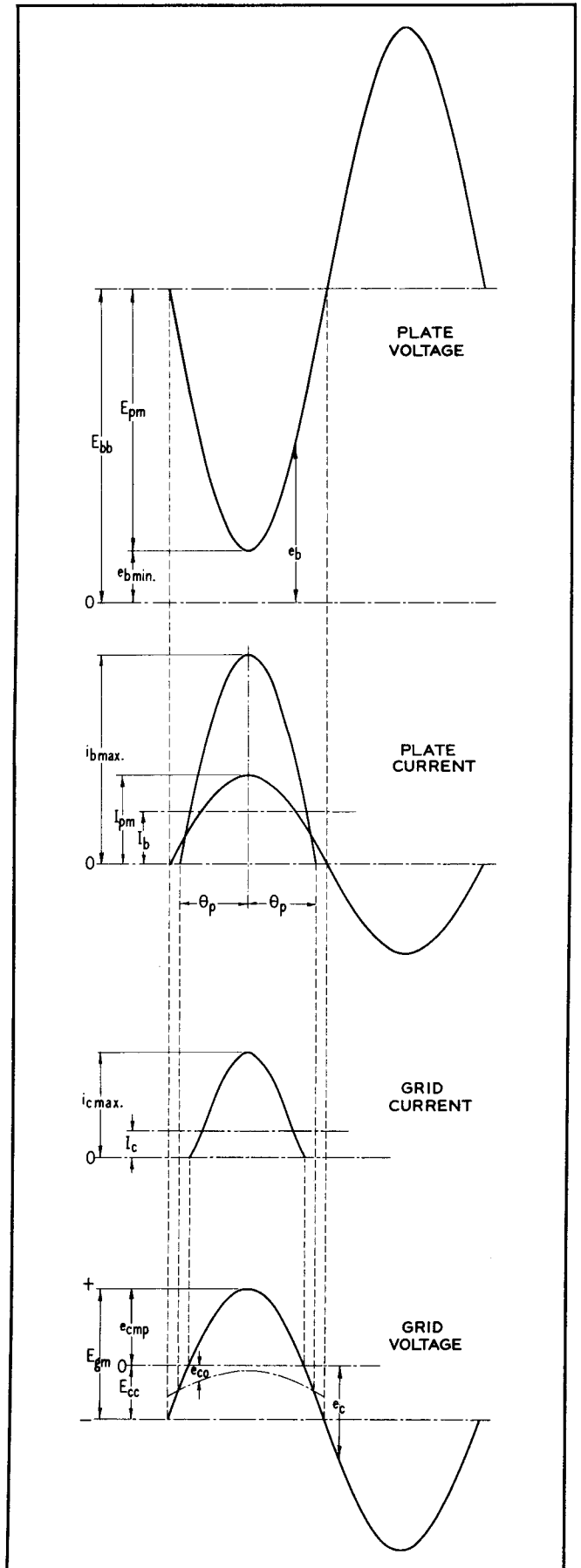


Figure 1. Symbols

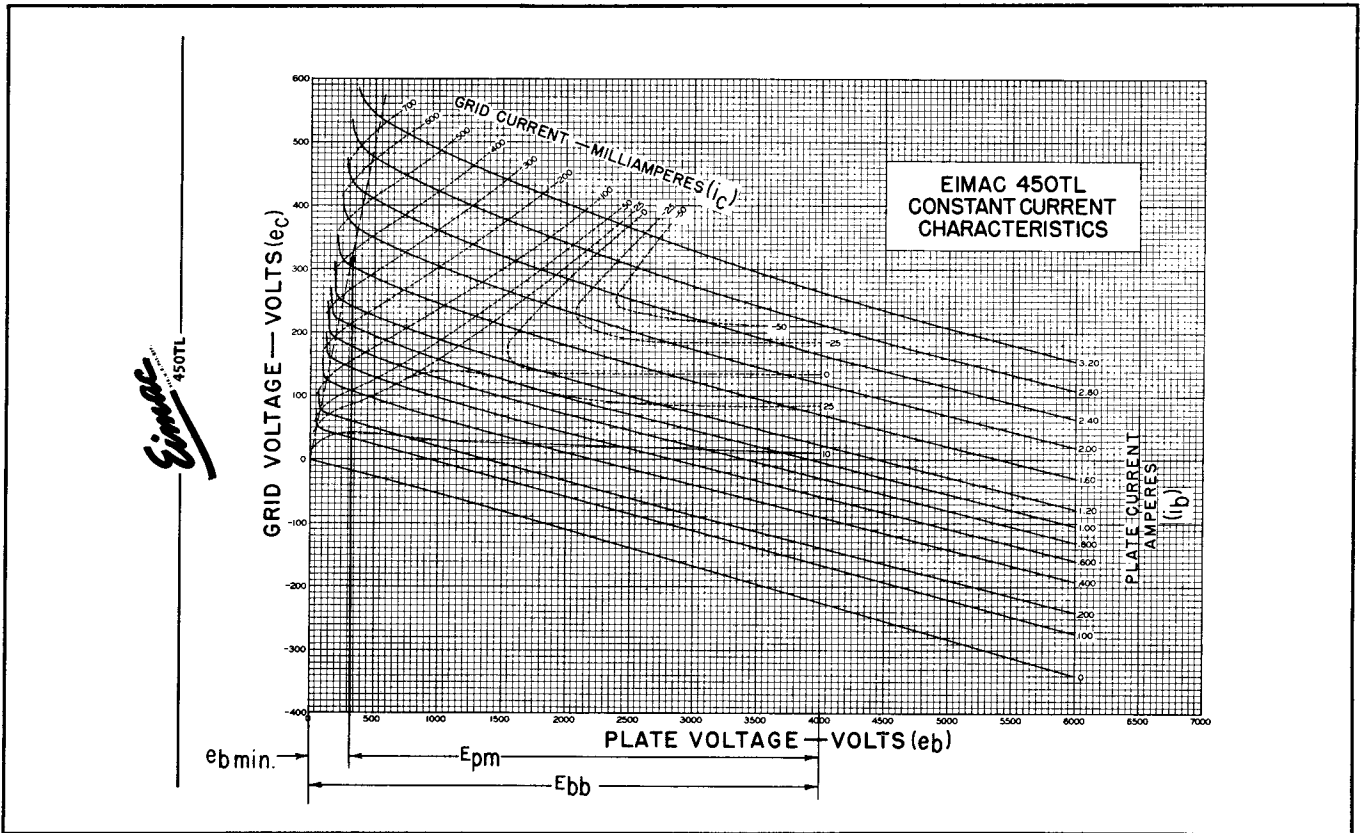


Figure 2. 450TL constant-current characteristics showing method of determining $e_{b\min}$ and E_{pm} in steps 6 and 7 from value of i_b obtained in step 5.

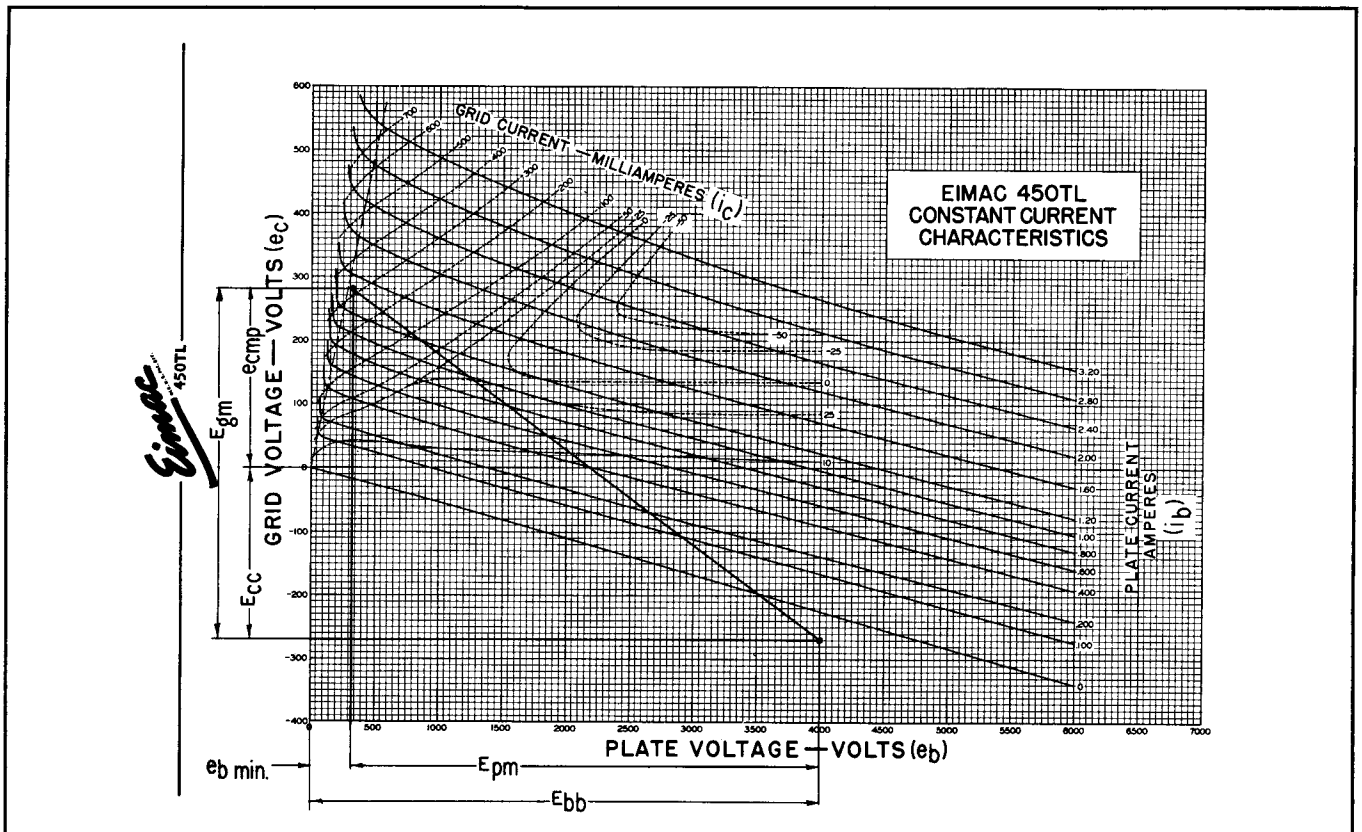


Figure 3. Method of determining e_{cmp} and i_c on 450TL constant-current characteristics from values of $e_{b\min}$ and E_{pm} found in steps 6 and 7 and value of i_b found in step 10. The value of E_{cc} and E_{gm} from steps 13 and 14 and the operating line are also shown.